# **Transformations of sulfur compounds in oil shale ash suspension**

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# **Abstract**

Oil shale (sulfur content  $\langle 2\% \rangle$ ) is mainly used for the production of electricity and heat in Estonia. Calcium-rich waste formed in the process of oil shale combustion can be used as sorbents in the  $CO<sub>2</sub>$  mineralisation process.  $CaSO<sub>4</sub>$  is the main sulfur compound in the ashes of oil shale, but traces of sulfides are also found. This means that transformations of sulfur compounds in the water environment must be considered while using hydrotransport and open air deposition of oil shale ash as well as treating alkaline ash transportation waters. The transformations of sulfur compounds in model systems (ash – water and CaS – water) were studied in anaerobic and aerobic conditions as well as in the process of aqueous carbonization. The separation of poisonous  $H_2S(g)$  was continuously monitored. The results revealed that the leachates of oil shale ash contained mainly sulfates in both aerobic and anaerobic conditions but sulfides and sulfites were also present. Small amount of  $H_2S(g)$  was emitted already in the first minutes of carbonation process at high pH region  $(\sim 12)$ . The alkalinity decreased during carbonation of ash – water suspensions, triggering substantial  $H_2S$  release at pH<9 (the content of  $H_2S(g)$  in off-gas reached to 110 ppm). Taking environmental issues into consideration, the critical pH value of the aqueous carbonation system of oil shale ash must be optimized in order to minimize the separation of gaseous  $H_2S$  emissions.

*Keywords: calcium sulfide, oil shale ash, mineral carbonisation, H2S.* 

# **1 Introduction**

Considering the importance of energetic safety, a local low-calorific fossil fuel oil shale (sulfur content  $1-2\%$ ), is used for heat power production in the



Republic of Estonia. The oil shale-fired power plants use pulverized firing (PF) as well as circulating fluidized bed combustion (FBC) technologies. The main contaminants are  $SO_x$ ,  $NO_x$ , particulate matter and  $CO_2$ . PF is related to relatively high  $SO_2$  emissions (concentration of  $SO_2$  in flue gases is  $\sim$ 2200mg/nm<sup>3</sup>) [1]. The majority of sulfur emissions pass over the sea, where they deposit as acid and mix with the water upper layers, decreasing the pH of seawater. The lower part of the sulfur emissions falls on continental soils and fresh waters downwind  $[2]$ . FBC eliminates  $SO<sub>2</sub>$  emissions almost completely; the latter is bound into solid mineral waste – oil shale ash (OSA) [3]. Most of the OSA is deposited in waste piles due to current lack of practical applications and becomes the source of solid, liquid and gaseous pollutants. Various studies have shown that leaching of the minerals and organics from OSA-s is a continuous and relatively long-term process, which means that the ash piles contaminate the environment for a long time  $[4–6]$ . CaSO<sub>4</sub> is the main sulfur compound present in the oil shale ashes, but also traces of sulfides are found [7, 8]. Series of reactions (eqns.  $(1)–(6)$ ), [5, 8, 9]) occur during ash contact with water and atmospheric components at open-air deposits, including release of gaseous hydrogen sulfide  $(H_2S(g))$  [3, 9] under certain conditions.  $H_2S(g)$  is an extremely toxic and irritating gas, which affects the nervous system, intermits breathing or impairs cardiac function. People can smell  $H_2S$  at low contestations 0.0005– 0.3 ppm, the sense of smell is disabled at concentrations 100-200 ppm, making it impossible to detect the compound. Rapid death ensues from exposure to more than about 1000 ppm  $H_2S$  due to asphyxiation [10, 11]. This means that transformations of sulfur compounds in the water environment must be considered while treating ash-water suspensions and ash transportation waters.

Atmospheric emissions of  $CO<sub>2</sub>$  originating from the Estonian oil shale are also a serious problem. A possible solution to reducing the negative environmental impact of emissions is  $CO<sub>2</sub>$  mineralization, so-called direct or indirect aqueous carbonation, which leads to abatement of  $CO<sub>2</sub>$  emissions ( $CO<sub>2</sub>$ ) binding potential is 200–250kg  $CO<sub>2</sub>/t$  OSA) as well as utilisation of OSA for precipitated calcium carbonate (PCC) production [4, 6, 12–14]. While the carbonation leads to changes of pH values of suspension the aim of current study was to investigate the transformations of sulfur compounds in the course of leaching (in anaerobic and aerobic environment) and aqueous carbonation of OSA (and CaS as a model compound) in order to bring out the environmental issues related to possible emissions of toxic  $H_2S$ .

## **2 Materials and methods**

In this study two types of model systems (OSA – water and CaS – water), in anaerobic  $(N_2)$  and aerobic (in air) conditions were investigated. The aim of aerobic conditions was to imitate the situation in the nature in case of open system, and there is air oxygen access to the suspension. The aim of anaerobic conditions was to imitate the same situation without the access of air oxygen, which takes place in the deeper layers of ash piles. CaS–H<sub>2</sub>O systems were used as a model in order to explain and simplify the CaS transformations taking place



in OSA-water system. Selected fraction of circulating fluidized bed combustion bottom ash (FBCA) collected from boilers at Estonian power plants was used in the present research. The main characteristics of OSA-s (FBCA and pulverized firing bottom ash (PFA)) [4, 12] including different sulfur forms are presented in table 1. Total sulfur and its bonding forms (sulfide sulfur, sulfate sulfur) in OSA-s were determined according to the Estonian standard EVS 664:1995 for solid fuels [15]. Pure (99.9%) CaS were supplied by Alfa Aesar (German).

Ash type	% of dry matter						Particle mean	Density	<b>BET</b> surface
	$\mathbf{D}_{\text{tot}}$	$S_{\text{sulfide}}$	$S_{\text{sulfate}}$	CaO <sub>tot</sub>	CaO <sub>fr</sub>	CO <sub>2</sub>	diameter (µm)	(g/cm <sup>3</sup> )	area $(m^2/g)$
<b>FBCA</b>	5.08	0.28	4.80	53.2	19.7	$\gamma$ $\tau$	26.5	۰	.76
<b>PFA</b>	1 <sub>7</sub>	0.05	12		30.0	8.3	250.0	2.83	5.26

Table 1: The main characteristics of OSA-s.

 In this context, there was focused on sulfur compounds, therefore, for further experiments were used FBCA. Equilibrium experiments were carried out in a laboratory-scale batch reactor with volume 800 ml using ash-millipore water suspensions by solid/liquid mass ratio 1/10. CaS suspensions concentrations were as follow (in g/L): 0.13, 0.25, 0.5, 1.5 and 2.8. Suspensions were wellmixed at room temperature and atmospheric pressure for 180 min., which was considered sufficient to reach equilibrium. The suspensions were preserved for 24 hours to monitor the behavior of the components for a longer time period. The dynamics of  $Ca^{2+}$ , OH,  $S^2$ ,  $SO_4^2$  and  $SO_3^2$  -ions was followed during 15-1440 min. Samples were taken with syringe and filtrated  $(0.45 \mu m)$ . The filtrate was analyzed for  $SO_4^2$ ,  $S^2$ ,  $SO_3^2$  (using a Lovibond Spectro Direct spectrophotometer),  $Ca^{2+}$  (titrimetric method ISO 6058:1984) and OH-(titrimetric method ISO 9963-1:1994 (E)). pH (Mettler Toledo GWb SG2) in the reactor were continuously monitored. Aqueous carbonation was carried out in a 100 ml glass filter absorber using  $CO<sub>2</sub>$  containing model gas (15%  $CO<sub>2</sub>$  in air, which imitates the  $CO<sub>2</sub>$  concentration in actual flue gases). Gas phase composition  $(H_2S, O_2, CO_2, SO_2)$  using flue gas analyzer Testo 350-S/-XL) and suspension pH were continuously monitored during the experiments. Suspensions were filtered and the solid residue phase was dried at 105ºC. The solid phases were analyzed for chemical composition (free CaO content (ethyleneglycol method) and  $CO<sub>2</sub>$  (ISO-10694, ASTM E 191597, DIN EN 13137)).

### **3 Results and discussion**

#### **3.1 L Transformations in FBCA – water and CaS – water systems**

#### **3.1.1 Anaerobic conditions**

Solid CaS dissolves in the water and dissociates (eqn.  $(1)$ ) to give sulfide ions which will hydrolyze and form hydroxide ions as a result (eqns. (2) and (3)).

$$
CaS(s) \leftrightarrow Ca^{2+}(aq) + S^{2-}(aq)CaS(s) \leftrightarrow Ca^{2+}(aq) + S^{2-}(aq) \qquad (1)
$$

$$
S^{2-}(aq) + H_2O(aq) \leftrightarrow HS^{-}(aq) + OH^{-}(aq)
$$
 (2)

$$
HS^{-}(aq) + H_2O(aq) \leftrightarrow H_2S(aq) + OH^{-}(aq)
$$
 (3)

 In the anaerobic systems of CaS – water the liquid phase contains mainly  $Ca<sup>2+</sup>$ , HS<sup>-</sup> (main sulfide form in the present pH [9]), and OH<sup>-</sup> - ions. When OSA is immersed into water, dissociation of forming portlandite  $(CaOH<sub>2</sub>)$ , eqn. (8) and dissolution of different salts (anhydrite, gypsum, calcite, dolomite, periclase) occur [14]. During the first minutes of CaS – water and FBCA – water contact, the solution becomes deeply alkaline  $(\sim 11.4$  and  $\sim 12.7$ , accordingly) and the pH stabilizes at these values, fig.1. The equilibrium is reached more rapidly in case of FBCA–H2O system. The pH of aqueous suspensions falls only a few units under anaerobic conditions. This is due to oxidation of sulfide ions, eqns.  $(4)$ ,  $(5)$ and (6) or the  $H_2S$  evaporation into the gas phase, eqn. (7).

$$
HS^{-}(aq) + 1.5O_{2}(aq) \leftrightarrow SO_{3}^{2-}(aq) + H^{+}(aq)
$$
\n(4)

$$
SO_3^{2-}(aq) + 0.5O_2(aq) \leftrightarrow SO_4^{2-}(aq) \tag{5}
$$

$$
SO_3^{2-}(aq) + 0.5O_2HS^-(aq) \leftrightarrow S_2O_3^{2-}(aq) + OH^-(aq) \tag{6}
$$

$$
H_2S(aq) \leftrightarrow H_2S(g) \tag{7}
$$



Figure 1: Changes in the pH in CaS–H<sub>2</sub>O and FBCA–H<sub>2</sub>O systems under anaerobic conditions.

 The oxidation of sulfides promotes pH decrease in the system, as the sulphates are weaker bases than the sulfides. Until there is sufficient amount of solid phase, the oxidation of sulfides does not affect the pH of the solution, as oxidized ions are replaced by the dissociation of CaS. The greater amount of initial CaS added into the water the greater the concentration of sulfides in the liquid phase. In contrast to aqueous suspensions of CaS the concentration of  $S<sup>2</sup>$ ions in aqueous phase kept growing continuously in case of FBCA. Sulfide ion

diffusion from the solid FBCA particle was slower and the equilibrium was not achieved within 24 hours, fig. 2. The content of sulphate ions in the liquid phase increased rapidly >1000 mg/L in case of FBCA – water system and stabilized after 3 hours (180 minutes). In case of the CaS suspensions the content  $SO_4^2$ ions increased steadily from 2 to 23 mg/L (CaS 0.5g/L) during 24 hours, fig. 3 due to leakages in the air-tight system, thus promoting the formation of sulfates. Sulfites content in FBCA leachates was lower compared to CaS, fig 4. Sulfites were probably formed during the analysis.



Figure 2: Changes in  $S^2$ -ion concentration in CaS–H<sub>2</sub>O and FBCA–H<sub>2</sub>O systems under anaerobic conditions.



Figure 3: Changes in  $SO_4^2$ -ion concentration in CaS-H<sub>2</sub>O and FBCA-H<sub>2</sub>O systems under anaerobic conditions.



Figure 4: Changes in  $SO_3^2$ -ion concentration in CaS–H<sub>2</sub>O and FBCA–H<sub>2</sub>O systems under anaerobic conditions.

#### **3.1.2 Aerobic conditions**

After dissociation of CaS the resulting sulfides bound protons in water so rapidly that the oxidation of solid phase is almost non-existent [9]. The results showed that the majority of sulfides oxidized to sulfites, and reduced sulfates. The aqueous suspensions could include polysulfides and thiosulfates which were not determined in this study; the latter may affects the results. In aerobic conditions the pH of the ash leachates increased higher more rapidly as compared CaSwater systems, fig. 5.



Figure 5: Changes in the pH in CaS–H<sub>2</sub>O and FBCA–H<sub>2</sub>O systems under aerobic conditions.

Thus, the formation of Ca and Mg hydroxides as well as dissolution, eqn. (8) and (9) was faster than the dissociation of CaS to cations and anions, eqn. (1), and following reaction between sulfides and protons, eqn. (2) and (3).

$$
CaO(s) + H_2O(aq) \leftrightarrow Ca(OH)_2(s) \leftrightarrow Ca^{2+}(aq) + 2OH^{-}(aq) \tag{8}
$$

$$
MgO(s) + H_2O(aq) \leftrightarrow Mg(OH)_2(s) \leftrightarrow Mg^{2+}(aq) + 2OH^{-}(aq) \qquad (9)
$$

 In case of lower CaS concentrations (CaS<1.5g/L) the dissociation of CaS was complete, during the 30 minute of CaS – water contact, so desorption and oxidation of sulfides could not be replaced on account of solid CaS and the system's pH decreases due to absorption  $O_2$  and  $CO_2$ . At higher concentrations (CaS>1.5g/L) the system reaches equilibrium and subsequent processes are slow. In FBCA – water system, within 24 hours, the concentration of  $S^2$ ,  $SO_4^2$  and  $SO_3^2$ -ions increase steadily, fig. 6, 7 and 8. Thus, after 24 hours of leaching the source of sulfides still remains. Days after, at lower concentrations (CaS<0.5g/L), the equilibrium was achieved and sulfites are partially oxidized to sulfates, fig.7 and 8. Diffusion of sulfides from the ash particle into solution took much more time as compared to pure CaS. In FBCA–H<sub>2</sub>O system the sulfates had already reached equilibrium after 3rd hour of leaching, as in case of CaS– H2O systems the concentration of sulfates in the liquid phase kept increasing, fig. 7. Diffusion of sulfates from ash was faster than the oxidation of sulfides to sulfates. Fewer sulfides formed into FBCA  $-H<sub>2</sub>O$  system than into CaS– $H<sub>2</sub>O$ system. Similarly to sulfides (fig. 6), due to oxidation of the latter, the content sulfites increases, fig. 8. Share of sulfites transform to sulfates, depending on the diffusion of sulfides into liquid phase.



Figure 6: Changes in  $S^2$ -ion concentration in CaS–H<sub>2</sub>O and FBCA–H<sub>2</sub>O systems under aerobic conditions.





Figure 7: Changes in  $SO_4^2$ -ion concentration in CaS–H<sub>2</sub>O and FBCA–H<sub>2</sub>O systems under aerobic conditions.



Figure 8: Changes in  $SO_3^2$ -ion concentration in CaS-H<sub>2</sub>O and FBC-H<sub>2</sub>O systems under aerobic conditions.

#### **3.1.3 Comparison of the results in anaerobic and aerobic conditions**

In both aerobic and anaerobic conditions the aqueous solutions became rapidly highly alkaline after the contact of ash and water, the pH remained stable upon the arrival of the equilibrium, fig. 1 and fig. 5. Thus, proton capture of sulfides, releasing OH<sup>-</sup>-ions into solution, eqn. (2) and (3), is preferred as compared to the oxidation of sulfides, eqn. (4-6).

In aerobic conditions  $(CaS<1.5g/L)$  than equilibrium, pH of the solution falls within 24 hours. Under anaerobic condition at higher CaS concentrations  $(CaS > 0.13g/L)$  the suspension liquid phase contained  $\sim$  twice as much OH<sup>-</sup>-ions  $(\sim 4$ mmol/L) as compared to Ca<sup>2+</sup>-ions ( $\sim 2$ mmol/L), as result of H<sub>2</sub>S in the solution which leads to the additional metallic sulfide dissolution according to eqn.  $(11)$ :

$$
H_2S(aq) + S^-(aq) \leftrightarrow 2HS^-(aq)
$$
 (11)

 Therefore, more hydrogen sulfide ions would be provided into solution and for equilibrium constants to remain the hydrogen sulfide ions have to bind more protons, resulting formation of H2S and remaining of more hydrogen ions in the solution. In case of anaerobic conditions the sulfides content in the liquid phase was lower, fig. 2, 5. Thus, the oxidation of sulfur compounds accelerates the dissolution of CaS. Although  $H<sub>2</sub>S$  releasing in gaseous form has an important role in solid phase dissociation, the slower dissociation of CaS was determined in anaerobic conditions. Desorption of  $H<sub>2</sub>S$  was suppressed in the presence of oxidants. Under aerobic conditions  $Ca^{2+}$ -ions content decreased, table 2, thus in oxidizing condition due to binding of the  $Ca^{2+}$ -ions (eqn. (8) and (13)), the solidification was beneficiary. Therefore contrary to the sulfides, the concentration of  $SO_4^2$ -ions was in every case higher under aerobic conditions fig. 3 and 7.

#### **3.2 Aqueous carbonation of FBCA and CaS**

Carbonation experiments showed that small amounts of H2S were emitted already in the region of high pH value ( $pH~12$ ) during the first minutes of carbonation process, fig. 9. The system pH decreases as model gas was bubbled through the aqueous suspensions of FBCA or CaS.  $CO<sub>2</sub>$  behaves as acid in the aqueous systems [14], eqn. (12):

$$
CO2(g) + H2O(aq) \leftrightarrow H2CO3(aq) \leftrightarrow H+(aq) + HCO3-(aq)
$$
 (12)

$$
Ca^{2+}(aq) + CO_3^{2-}(aq) \leftrightarrow CaCO_3(s)
$$
 (13)

During carbonation, in case of CaS–H<sub>2</sub>O system, pH decreases faster and to lower values, than in FBCA–H<sub>2</sub>O system, fig. 9. In case of CaS the pH reached equilibrium ( $pH~6.3$ ) in 5 minutes, as in case of FBCA system in 30 minutes (pH~6.8). In FBCA system pH stayed on a high level until almost all free lime (CaO) was utilized (as long as calcium was carbonated). In CaS–H2O system the pH decreased rapidly because of lack of CaO. pH decrease favors the evaporation of H<sub>2</sub>S, which also earlier studies refer [14]. When the suspension pH decreased below 7.5, the content of  $H_2S$  in off-gas reached 110 ppm in case of FBCA and  $>1500$  ppm in case of CaS (CaS 0.6g/L). Release of the H<sub>2</sub>S stopped in correlation with the respective source of sulfide. Thus, at pH values  $\leq$ 10 desorption of gaseous H<sub>2</sub>S is preferred to oxidation of sulfides, which was expressed by the intense emission of  $H_2S$ . Determination of solid phase composition indicated that over 85% of free lime (content of free CaO  $\langle 2\% \rangle$ ) was utilized before reaching into the intensive  $H_2S_g$  emission region (pH<9) during aqueous carbonation of OSA. The amount of  $CO<sub>2</sub>$  bound was 210kg  $CO<sub>2</sub>/t$ FBCA.





Figure 9: Changes in the composition of off-gas and suspension pH during aqueous carbonation of FBCA.

### **4 Conclusions**

Experiments in model systems showed that transformations of the sulfur compounds in the water environment must be considered while using hydrotransport and open air deposition of oil shale ash as well as treating alkaline ash transportation waters.  $H_2S$  has an important role in CaS dissociation. As long as there is a solid CaS in the system, the source of sulfides,  $O_2$  and  $CO_2$ absorption does not affect the oxidation of sulfides and suspensions pH decrease The kinetic desorption of gaseous  $H_2S(g)$  is preferred to oxidation of sulfides when suspension pH<10. Taking environmental problems into consideration, the pH of the aqueous carbonation system of OSA must be monitored – the separation of highly toxic gaseous  $H_2S(g)$  can be minimized by optimizing pH value of the system. Carbonation should be discontinued at the time when no more  $CO<sub>2</sub>$  is committed by the amount of free CaO in the OSA, thus preventing a rapid pH decrease of the system.

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