CALCIUM EXTRACTION FROM ESTONIAN INDUSTRIAL WASTES BASED ON AMMONIUM SOLVENTS

KADRIANN TAMM, REGIINA VIIRES, REIN KUUSIK & MAI UIBU Laboratory of Inorganic Materials, Tallinn University of Technology, Tallinn, Estonia

ABSTRACT

In Estonia electricity production is based mainly on local oil shale, the latter has been the country's most important mineral resources throughout the last century, up to today. In addition, the municipal solid waste incineration (MSWI) based heat and power production has developed rapidly. Industrial wastes from combustion processes are often rich in calcium and could be used as raw materials for CO₂ sequestration and calcium carbonate production. Batch dissolution experiments were carried out to investigate Ca extraction from industrial wastes using ammonium salt solvents (NH4Cl, NH4NO₃ and CH₃COONH₄). The dissolution equilibrium and dynamics of the main species was studied from the aspects of Ca extraction selectivity and environmental safety. Conductivity and pH change in the studied systems depends mainly on the solvent (its electrolyte ionic strength and ion mobility), addition of ashes basifies the systems. Test results indicated that Ca²⁺ ion extraction was noticeably enhanced by ammonium salts as compared to water systems, using NH4NO₃ solution gave the best results (extraction degree up to 95%). A simplified leaching mechanism for ash-solvent systems was presented, the latter can be used for future theoretical calculations. The study was focused on recovering of Ca from Estonian waste ashes, development of calcium carbonate as a commercial by-product will be the next step.

Keywords: oil shale ash, municipal solid waste incineration ash, precipitated calcium carbonate, utilization, CO_2 sequestration.

1 INTRODUCTION

Republic of Estonia processes annually about 20 million tons of local fossil fuel, oil shale (OS), producing over 6 million tons of OS ash from heat and power generation as well as shale oil production [1]. Substantial waste flows are also linked with industrial processes such as municipal solid waste incinerator (MSWI) - 56,000 tons/y of bottom ash, 3,800 tons/y of fly ash (FA) and 6,500 tons/y of air pollution control (APC) residue [2]. Reuse of these wastes is currently very limited in Estonia - only 5% of OS ashes are utilized mostly in the cement industry, the rest of it is deposited in ash fields. In addition, 11,5 Mt of CO_2 was emitted in 2016 from the power plants, of whose OS combustion has the biggest proportion due to the high content of mineral carbonates in OS [1], [3]. Recycling of these wastes is obligatory in order to move towards circular economy.

It has been demonstrated that an OS ash–water suspension is able to bind up to 290 kg of CO_2 per ton of ash [4]. Moreover, upgrading industrial wastes into commercial products (e.g., precipitated calcium carbonate (PCC)) [4]–[7] via the carbonation route is one of the promising directions for CO_2 sequestration process. In recent years, various carbonation routes have been studied in various reactor configurations to produce PCC-type materials using both industrial ash and its leaching waters that are saturated with calcium and accompanying ions [8]–[11].

Studies have shown that $Ca(OH)_2$, $CaSO_4 \cdot 2H_2O$ and CaS are the main water-soluble Ca and S species in OS ash aqueous systems [12]. Also, OS ashes contain secondary Ca(Mg)silicate minerals, and an amorphous Al-Si glass phase [4]. Estonian MSWI residues are hazardous solid wastes since they include heavy metals and organic pollutants in addition to metal oxides and water-soluble salts [13]. The latter influences the chemical composition of



ash-water leachates. For PCC purity, it is essential to ensure the efficient but also selective extraction of calcium ions. It has been found that ammonium salts, NH₄Cl, NH₄NO₃ and CH₃COONH₄, solutions were the most promising solvents for selective extraction of calcium from steel slags [14].

The current study focuses on Ca extraction from OS and MSWI ashes using ammonium salt solvents. The dissolution equilibrium and dynamics of the main species was studied from the aspects of Ca extraction and environmental safety.

2 METHODOLOGY

Batch dissolution experiments were carried out to investigate Ca extraction from industrial ashes using ammonium salt solvents (NH_4Cl , NH_4NO_3 and CH_3COONH_4) and acetic acid (CH_3COOH) of 2M concentrations.

2.1 Characterization of materials

Oil shale fly ashes (CFB1, CFB2 and PF) collected from Narva Power Plants and shale oil production (Enefit 280) as well as the air pollution control residue (APC) and fly ash (FA) from municipal solid waste incineration block in Iru Power Plant were tested for Ca extraction. The circulating fluidized bed ashes CFB1 and CFB2 were taken from the common silo and from the first field of electrostatic precipitator at 2011 and 2016, respectively. The pulverized firing cyclone ash PF was collected in 2011, the Enefit280 fly ash and MSWI ashes in 2016. Ash samples were analysed using both X-ray fluorescence spectroscopy (XRF, Rigaku Primus II) and quantitative X-ray diffraction (XRD, Bruker D8 Advanced) methods at the Institute of Geology, University of Tartu. The contents of free lime (CaO_{free}) (ethylene glycol method) [15], sulfur (as sulfate) [16], total carbon (TC) (Electra CS - 580 Carbon/Sulfur Determinator) were determined. The BET specific surface area (SSA) and the particle size distribution analyser LA-950, respectively. The chemical composition as weight percentages together with the physical characteristics of the ashes are provided in Table 1.

Chemical data	Oil shale ashes				MSWI ashes	
	CFB1	PF	CFB2	Enefit280	APC	FA
Experimental						
CaO _{free}	12.31	22.37	12.00	0.36	10.02	5.49
CO ₂	11.11	1.10	5.31	16.83	6.35	3.58
S _{SO4}	7.90	5.24	1.93	2.26	2.49	1.53
XRD/XRF						
SiO ₂	26.06	21.11	23.96	25.99	8.52	31.9
CaO _{tot}	36.25	49.59	37.25	33.48	29.82	32.02
MgO	3.94	3.30	2.43	1.98	1.81	3.10
Na ₂ O	0.07	0.04	0.11	0.09	19.00	4.61
K ₂ O	3.29	2.04	3.93	3.81	12.21	3.92
CO _{2max}	18.95	15.88	13.47	17.06	13.19	7.57
Physical characteristic						
SSA, $m^2 \cdot g^{-1}$	6.30	0.40	4.75	4.24	7.88	1.2
d _{mean} , μm	26.5	61.73	16.84	36.4	20.99	-

Table 1: Characterization of industrial waste materials.



The characteristics of ashes is highly dependent on the combustion technology. Of the six ashes, Enefit280 and FA ashes are characterized by the lowest free lime (CaO_{free}) content, other ashes are rich in CaO_{free} (>10wt%) (Table 1). The sulphur content in OS and MSWI ashes is present mainly in the form of anhydrite (CaSO₄). It has been shown that the smaller particle size of steelmaking slag, with a larger contact area available to react with the solvent, promoted Ca²⁺ ion extraction [17]. The OS ash leaching tests also indicated that the low leachability of calcium and sulfur species could be attributed to the coarse particle size of ash [18]–[19]. Effectiveness of the carbonisation process can be described by a maximal possible CO₂ content of the sample (CO_{2max}), which indicates that highest binding capacity (basis of the CO₂ and CaO content in the initial sample) has CFB1 ash and lowest MSWI FA.

2.2 Experimental procedure

All experiments with ash-solvent systems were performed at room temperature and atmospheric pressure by applying the standard batch-leaching test [20]. For kinetic studies, the leaching experiments were carried out in a laboratory-scale batch reactor with a volume of 200 ml. Ash-solvent suspensions were well-mixed, with a magnetic stirrer (700 rpm), The system pH (MT SevenGo pH) and electrical conductivity of the suspensions (MT SevenGo Duo Pro) were monitored during the experiments. To achieve an equilibrium state, the ash/solvent (1/10) systems under study were kept in 50 mL centrifuge tubes sealed with airtight caps for 24h in an overhead shaker (GFL 3025) at 45 rpm throughout the experiment. The suspensions were filtered using a vacuum filter (Munktell filter paper, 100 g/m²). The filtrates were analysed for cations, anions and heavy metals content. The content of sulfate and sulfide ions was determined using a Lovibond Spectro Direct spectrometer (barium sulfate turbidity and DPD/Catalyst methods, respectively). The cations (Ca²⁺, Mg²⁺, Na⁺ and K⁺) and heavy metals (Zn, Pb, Cd and Cr) were determined by atomic absorption spectroscopy (Carl Zeiss Jena AAS IN: Verian Spectra AA 55B).

3 RESULTS

3.1 Solubility results in ash-solvent systems

The pH, conductivity, and the concentration of the main species in the liquid phase was determined in ash-solvent equilibrium systems (1/10 and 1/50) by varying the type of ash as well as the solvent.

3.1.1 Systems pH

It has been shown that extraction efficiency is not the only factor to affect the process, the favourable pH conditions crucial to guarantee the carbonisation efficiency in the final step [21].

The pH of systems were measured before and after extraction to detect the pH change (Fig. 1). The analysis results indicated that Ca concentration increased with the solid to liquid ratio from 1/50 to 1/10 up to 25000 mg/L in acidic acid systems and ranged between 1000-4000 mg/L in ammonium salt systems. The changes in water systems were less noticeable (up to 500 mg/L) due to much lower solubility of portlandite in water. Increasing S/L ratio to 1/5 in OS ash-water systems had no effect in Ca leaching [12].

The average pH increase in 1/10 ash-NH₄Cl and ash-NH₄NO₃ systems were <5 units, and for acetate systems <3 units, almost twice the growth. Thus, the final pH of the ash-solvent system was rather affected by the selected solvent than the characteristics of the ash.



Figure 1: The pH of 24 h ash/solvent (1/10) system.

The lowest pH was determined in Enefit280-solvents systems, in which case the ash contained the lowest amount of CaO_{free} was lower (Table 1).

For all ash-solvent system pH was noticeably lower than for ash-water systems (pH \sim 12), which may affect the further carbonisation process.

3.1.2 Systems EC

When ash was immersed info ammonium salt solvent, the electrical conductivity (EC) decreased as, shown in eqn. (1)–(3), mobile hydroxonium ions (349.8 S·cm²/mol) are replaced by less mobile ions, (e.g. Ca²⁺ ion (59.5 S·cm²/mol) or OH⁻ ion (198.3 S·cm²/mol [23]). In acetic acid systems, the dissolved ion content and interactions are small, with the addition of ash the electrical conductivity increased because the weakly dissociated acid is replaced by the highly dissociated compounds during neutralization.





Figure 2: Electrical conductivity of 24 h ash/solvent (1/10) system.

The electrical conductivity was higher in case of all the selected solvents as compared to ash-water systems, even for APC ash-solvent systems, which contained mainly water-soluble Ca compounds (Ca(OH)₂, CaCl(OH), CaO).

3.1.3 Leachability of cations and anions in ash-solvent systems

From the aspect of PCC purity, it essential to investigate the leaching of dissolvable species in ash-solvent systems.

Using acidic acid resulted highest the concentration of Ca^{2+} ions in the filtrate (32000 mg/L), but the concentration of cations (Mg²⁺, K⁺ and Na⁺) and anions (SO₄²⁻, S²⁻, Cl⁻, SiO₂) was also high (Fig. 3 and Fig. 4). Also, the CFB2 leachate contained heavy metals Zn and Pb, 56.8 and 5.12 mg/L, respectively.

When ammonium solvents were used, the Ca concentration (up to 20000 mg/L) was higher as compared to ash-water systems but the leaching of other components was inhibited (except for sodium and potassium). All of the ash-solvent filtrates contained Mg^{2+} ions, unlike ash-water systems, where the concentration of magnesium ion was negligible.



Figure 3: Concentration of Ca^{2+} and Mg^{2+} ions in 24 h ash-solvent systems.



Figure 4: Concentration of sulfur ions in 24 h ash-solvent systems.

The results indicated that calcium could be selectively extracted from OS and MSWI ashes using ammonium solvents.

3.2 Dissolution kinetics in ash-solvent systems

The main characteristics of the Ca dissolution process for OS ashes and the dissolution kinetics of main water-soluble Ca-compounds together with the dissolution mechanism has been described in previous studies [12], [24], [25].

As the system pH and electrical conductivity had similar changing dynamics in case of all selected ashes indicating that the main changes occurred in 1 minutes, the main results are shown based on CFB OS ash on Fig. 5, Fig. 6, Fig. 7 and Fig. 8.

As the ash was contacted with the solvent, dissociation of the compounds occurred immediately leading to the increase in hydroxide ions concentration expressed in the rapid pH increase of the suspension.



Figure 5: The pH change of CFB OS ash-solvent system pH up to 10 minutes $1/10 (\Delta)$ and $1/50 (\bullet)$.



Figure 6: Changes in system pH for CFB OS ash-solvent system during 1 minute.



Figure 7: Changes in electrical conductivity for CFB OS ash-solvent during 10 minutes $1/10 (\Delta)$ and $1/50 (\bullet)$.



Figure 8: Changes in electrical conductivity for CFB OS ash-solvent systems during 1 minute.

Calcium extraction reactions were completed within 1 minute, pH and conductivity change plateaued already in 10 minutes (Fig. 5 and Fig. 7). Using ammonium salt solutions induces a rapid decrease in electrical conductivity, as the use of acetic acid solution leads to its increase (Fig. 8).

The changes in electrical conductivity and pH in studied systems mainly depends on the solvent (NH₄Cl, NH₄NO₃, CH₃COONH₃, concentration 2M, its electrolyte ionic strength and ion mobility), addition of ashes basifies the systems.

3.3 Process chemistry

Eqns (1)–(4) represent a simplified dissociation for ash-solvent systems:

$$NH_3 + Cl^- + H_3O^+ + CaO \rightleftharpoons NH_4^+ + 2OH^- + Cl^- + Ca^{2+}.$$
 (1)

$$NH_3 + NO_3^- + H_3O^+ + CaO \stackrel{\sim}{\leftarrow} NH_4^+ + OH^- + NO_3^- + Ca^{2+}.$$
 (2)

$$NH_3 + CH_3COO^- + H_3O^+ + CaO \rightleftharpoons NH_4^+ + 2OH^- + CH_3COO^- + Ca^{2+}.$$
(3)

$$CH_3C00^- + H_30^+ + Ca0 \rightleftharpoons CH_3C00^- + Ca^{2+} + 2H_20.$$
(4)

CaO represents all water-soluble Ca regardless of the actual form in which it is initially bound. The two-weak base - strong acid salts (ammonium chloride and ammonium nitrate) eqns (1) and (2), a salt of a weak base and weak acid (ammonium acetate) eqn (3) and weak acid (acetic acid), eqn (4) represents the equilibriums states. This simplified ash-solvent leaching process chemistry can be used for future theoretical calculations.

3.4 Ca extraction efficiency

As shown in paragraph 3.3, the pH and electrical conductivity stabilised already during 10 minutes of contact, also the Ca extraction efficiencies remained constant after 10 minutes. The calcium ion extraction efficiencies for different solvents are shown in Fig. 9. For all ashes at 1/10 solid to liquid ratio the extraction efficiencies were higher with ammonium salt and acetic acid solvents compering water in all six ash systems.



Figure 9: Ca extraction efficiency according to solvent type.



Figure 10: Ammonium salts and acetic acid solvents vs water Ca extraction.

The extraction efficiency for ammonium salt solvents appeared to be in the same range in different ash systems (Fig. 9), about 70% in APC systems, 30% in FA systems, 50% in CFB2 systems, 21% in Enefit280, 15% in CFB1 and up to 50% in PF systems. The calcium was extracted most efficiently with acetic acid, up to 90%, however other species were detected in the filtrate as well, which could react with CO_2 and reduce the purity of PCC.

Comparing the extraction efficiency of ammonium salts and acetic acid solvents with water based systems, it was indicated that Ca extraction efficiency could be increased by 95% (Fig. 10). According to the main characteristics of initial ashes, e.g. CaO content, SSA, particle size, other water dissolved species, using CFB2 ash gave the best results.

4 CONCLUSION

Industrial wastes from combustion processes are often rich in calcium and could be used as feedstock for CO_2 sequestration and following calcium carbonate production. In order to use industrial wastes from combustion processes for CO_2 sequestration and further carbonisation, understanding the principles of Ca extraction is crucial. Batch dissolution experiments were carried out to investigate Ca extraction from OS and MSWI ashes using ammonium salt solvents. The dissolution equilibrium and dynamics of the main species was studied from the aspects of Ca extraction selectivity and environmental safety.

Results were compared with the previously studied ash - water systems. The system electrical conductivity and pH were continuously measured in order to follow the kinetics. The changes in respective indicators mainly depend on the solvent type (NH₄Cl, NH₄NO₃, CH₃COONH₃, concentration 2M, its electrolyte ionic strength and ion mobility), addition of ashes basifies the systems.

Test results indicated that Ca²⁺ ion extraction was noticeably enhanced by ammonium salts solutions as compared to water based systems, using NH₄NO₃ solution gave the best

results (extraction degree up to 90%). A simplified leaching mechanism for ash-solvent systems was presented, the latter can be used for future theoretical calculations.

This work examined the extraction of the Ca^{2+} ion as the first step of the complex mineral waste utilisation process. These results would serve as basis for the further studies, which focus on the carbonisation processes of the respective extracts and its effect on process conditions and the quality of PCC as commercial product.

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