The flushing of pollution from recreational boating in tidal embayments with application to Great Salt Pond on Block Island

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Abstract

Pollution loading from recreational boating has been gleaned from seasonal boat count data, published results of pollutant releases from marine engines, and boat type and size distributions from marine association data. These loading functions have then been used in the single-basin MSB model of pollution-flushing, a systems-dynamic model written in Stella (Stella is a product of ISEE Systems, Inc., formerly High Performance Systems of Hanover, New Hampshire, USA), which has been validated in tank tests and in a specific application to Great Salt Pond on Block Island. The results of the present study allow the concentration of various aqueous pollutants associated with the propulsion component of recreational boating to be computed in well-mixed tidal embayments.

Keywords: tidal prism, pollution flushing, tidal embayment, recreational boating pollution, Great Salt Pond Block Island.

1 Introduction

While coastal embayments are likely to benefit from 'no discharge' regulations, recreational boating adds a number of pollutants from marine engine use to basins that serve as harbors for these vessels. The MSB single-embayment model [1] offers a graphical and numerical representation of the process of pollution flushing from well-mixed tidal embayments. The model, which is written in Stella (Stella is a product of ISEE Systems, Inc., formerly High Performance



Systems of Hanover, New Hampshire, USA), allows for realistic basin bathymetries, cascading basins [2] as well as the dynamic loading of pollutants [3]. The governing rate equations driving the model are the same as those found in the analytical tidal prism model developed by Barber [4] for constant pollution loading and simple basin geometries. The governing equations are derived from the following mass flow equation:

$$\frac{d(CV)}{dt} = V\frac{dC}{dt} + C\frac{dV}{dt} = QC + k \tag{1}$$

where Q is the discharge through the mouth of the embayment and k is the pollution loading rate, which may be time-dependent. During the ebb flow period, dV/dt = Q, allowing the QC term on the right-hand side of eqn. (1) to be cancelled with the CdV/dt term on the left. During the flood flow period, the QC term on the right-hand side of the equation can be assumed to be zero, provided the pollution return-flow rate into the basin is ignored. This results in two rate equations for dC/dt, one for the ebb and another for the flood conditions.

One of the crucial parameters in the MSB model is the pollution return-flow factor, b. This parameter is used to modify the volume of the tidal prism to account for the return of polluted water during the flood tide. This methodology has been discussed by Barber [4] and more theoretically by Sanford *et al.* [5]. The volume-modifying factor is taken as (1-b), where b varies between 0, for no return flow, and 1, for total return flow. The MSB model [1] employs the basic state variable approach used in systems dynamics to represent the governing mass flow rate equations, treating the time-varying pollutant concentration, C, in the embayment as a level. The model has been validated against analytical and experimental data [4] and more recently has been applied to Great Salt Pond on Block Island, where in 1986 a Rhodamine dye study was conducted [6,7]. The results provide the first real basin validation of the MSB model.

The present paper extends the MSB model to study the flushing of pollutants associated with marine engines involved in recreational boating and applies the model to Great Salt Pond on Block Island where boat counts were graciously provided by the Harbourmaster and the Harbour Office. Pollutant data was gleaned from a number of studies [8-16] and coupled with boat type- and length-distributions, the model was expanded to define an appropriate loading factor, k, for the pollutant under consideration. An interface was written to allow for these factors to be changed for different embayments and boating data. Results for a typical season are presented for Great Salt Pond.

2 Great Salt Pond and boating data

Great Salt Pond is situated on Block Island, which is part of the State of Rhode Island and situated in the Atlantic Ocean at the entrance to Long Island Sound at a latitude of 41.191° N and a longitude of 71.575° W. The population of Block Island is little more than 1000 but this swells to 10,000 or more during the summer. Much of this increase is related to boating activities around Great Salt Pond, the bathymetry of which is shown in Figure 1.





Figure 1: Bathymetry of Great Salt Pond, Block Island and the dye release position (●) used in the pollution flushing study [7]. The chart has been overlaid with a grid in order to acquire the depth data for the MSB pollution-flushing model. Reproduced from NOAA chart number US 13217.

Annual seasonal boat counts on Great Salt Pond have been rather constant since a precipitous drop in 1996. These data are shown in Figure 2.

For purposes of illustration in this study, the 2004 boat count data were used and these are shown in Figure 3.

The peaks noted in this data correspond to weekends and holidays during the recreational boating season.

3 Extension of the MSB model to account for the pollutant loading associated with recreational boating

The factor, k, in eqn. (1) represents the embayment pollution loading rate expressed in terms of a mass per unit time. The literature provides results of a



Figure 2: Annual seasonal boat counts for Great Salt Pond.



Figure 3: Seasonal boat count data for 2004 smoothed with a spline function.

number of studies on the pollutants associated with marine engine use [8-16]. Four of these studies [8,9,10,16] were considered in the analyses reported herein. The pollution is often reported in grams of pollutant per horse-power hour with measurements being carried out for specific engine size and type and operating on specific vessel types and sizes. The array of boat types, hull shapes and engines will affect these pollutant values. A sample of the reported data used in the pollution loading section of the model is summarized in Table 1.

For a particular pollutant of mass, m_i , in g/hp-h, the pollution loading factor for an engine type, *i*, can be defined as

Table 1:Some common pollutant emissions associated with marine engine
use computed using data from reference [8]. While other data for
gasoline engines [9,10] were considered, only that from [8] were
used to obtain these results.

Emissions (g/hp-h)						
Pollutant	2-stroke	4-stroke				
HC (g)	240	12				
NMOG (g)	256	12				
CO (g)	488	142				
NO(x)(g)	0.89	5.8				
PM (10 micrometers)*	0.00604	0.00003				
PM (2.5 micrometers)*	0.00604	0.00002				
1,3 butadiene (g)	0.34	0.1				
benzene (g)	2.98	0.4				
benzene (aq)	0.16	0.052				
formaldehyde (g)	0.21	0.045				
acetaldehyde (g)	0.05	0.0075				
MTBE (aq)	5.15	0.22				
toluene (aq)	0.52	0.089				
ethylbenzene (aq)	0.15	0.022				

Notes:

[8] Two 9.9 Hp outboards, a 2-stroke Evinrude and a 4-stroke Honda, were tested in a 757 litre test tank of water. Test cycle included five modes: mode 1=full speed, 2=.8 speed, 3=.6 speed, 4=.4 speed, 5=idle. Each mode was run for ten minutes and a weighting factor was imposed to account for the varying amounts of fuel consumed by each mode. A weighted average emission rate for each pollutant was then determined from the emission rates at each mode and the weighting factor. Data analysis tools included infrared lasers, chemiluminescent analyzers, chromatography, and isokinetic sampling. Results in g/kW-h were converted to g/hp-h.

*Tested with both a PM10 and a PM2.5 cyclone.

[9] Two Yamaha 4-stroke outboards (15 Hp and 8 Hp) were tested with gasoline and commercial butane. Test cycle included five modes: mode 1=full speed, 2=.8 speed, 3=.6 speed, 4=.4 speed, 5=idle. Each mode was run for the same amount of time and a weighting factor was imposed to account for the varying amounts of fuel consumed by each mode. A weighted average emission rate for each pollutant can be determined from the emission rates at each mode and the weighting factor. Gas analyzers used: Horiba Mexa 574GE NDIR, Horiba FIA-510 CLD, Horiba CLA-510SS FID. Results in g/kW-h were converted to g/hp-h.

[10] One four-stroke Yamaha 9.9 Hp (7.3 kW) outboard engine was tested in an 800 litre tank of water. Average rpm=5600. Runs averaged 10-15 minutes on stand mounted to tank. Results given in mg/10 min may be converted to g/hp-h based on estimates of average power output corresponding to the test engine size and rpm. Data analysis tools included gas chromatography and mass spectrometry.

$$k_{i} = f_{i} \cdot BC_{total}(t) \cdot m_{i} \cdot \sum_{BLR=1}^{4} g_{i,BLR} \cdot hphbl(BLR) \cdot D$$
(2)

where the subscript *i* refers to the engine type with:

- 1 = inboard and auxiliary inboard
- 2 = 2-stroke outboards and auxiliary outboards
- 3 = 4-stroke outboards, auxiliary outboards and stern drive inboard-outboards
- 4 = personal water craft (PWC) engines

the subscript BLR refers to the boat length range with:

$$1 = 0$$
 to 16 ft

- 2 = 16 to 26 ft
- 3 = 26 to 40 ft
- 4 = 40 + ft

 f_i = fraction of boats with engine type, *i*,

 $BC_{total}(t) =$ total daily boat count at time, t (days)

 $g_{i,BLR}$ = fraction of type *i* engine boats in the length range, *BLR*

hphbl(BLR) = average computed hp-hr energy required to move a boat of length range, *BLR*, a distance of 1 mile at the posted speed limit (5 mph), and

D = average distance travelled during a boat's stay in the embayment.

Eqn. (2) was computed using the array functions within Stella and a user interface was written to allow for convenient definition of input requirements and ready update of pollution values as the literature develops. The total pollution loading rate, k, is simply the sum of the individual values of k, i.e.

$$k = \sum_{i=1}^{4} k_i \tag{3}$$

The model structure and the interface are shown in Figures 4 and 5, respectively. Tracking individual vessels and determining the daily mix of vessel types in the basin is not practical and hence the model uses estimates of average distance travelled per vessel during a daily stay and profiles of boat registrations to set the distributions, f and g, in eqn. (2).

4 Application of the model

In applying the model to Great Salt Pond, the value of the pollution return-flow factor, b, was set to 0.25 in accordance with the results from a previous study [6]. Bathymetric data and known tidal data for Great Salt Pond were used in the MSB model. Boat count data for 2004, as shown in Figure 3, were incorporated into the calculation of the pollution loading factor, k, from eqn. (2). While the boat count data did not differentiate on vessel type, size, and engine type and size, these distributions were obtained from registration and sales reports from the National Marine Manufacturers Association [17] and are summarized in Table 2.

The model application assumes each vessel moves at a speed of 5 mph, the maximum allowable limit, and travels a total of 1 mile each day within the limits of the basin. This would correspond to an average distance from entrance to anchorage/mooring/dockage and back each day.





Figure 4: Model structure showing both the MSB and pollution loading segments.



Figure 5:

User interface for the model.



Table 2:	Assumed distribution of boat power types by boat length range
	[17]. (Total percentage of all boats is a little higher than 100% due
	to round-off errors.)

LOA (ft)	Percent of all boats	Inboard/ Auxiliary Inboard	Outboard/ Auxiliary Outboard	Sterndrive	PWC	
0-16	43.73%	4.00%	31.81%	1.32%	6.60%	
16-26	51.95%	6.40%	34.11%	11.44%	0%	
26-40	4.00%	1.80%	0.96%	1.24%	0%	
40+	0.60%	0.41%	0.08%	0.11%	0%	





5 Results

A particular pollutant, ethylbenzene, was chosen in the present study. The pollution loading rate was calculated from eqns. (2) and (3) with m_i determined by weighting aqueous ethylbenzene emissions for the various engine types using a distribution reflecting that 96% of all engines are gasoline of which 45% are 4-stroke. Figure 6a represents the aggregate pollution loading rate as a function of the day of the boating season, with day 1 being defined as May 1. The concentration in g/m³ was simulated for the boating season using the MSB model driven by the pollution loading function and the results are shown in Figure 6b. Not surprisingly, the pollution concentration appears to follow the pollution loading rate in these results.



The obvious periodicities prompted a Fourier analysis of the time series. Indeed the results, shown in Table 3, clearly align with the principal harmonic components of the tidal spectrum [18]. The C/k spectrum exhibits other peaks corresponding to excursions in the time series that are the result of the flushing conditions of the embayment environment including the return flow and the pattern of pollution loading. Such spikes represent a short-term pulse in pollution concentration above what would normally be expected from the pattern of pollution loading based on boating activity at the time of the pulse.

<u>Tidal components – </u>	<i>C/k</i> frequency			
Component	T(hrs)	T(days)	f(1/days)	f(1/days)
principal lunar semidurnal	12.42	0.5175	1.932367	1.93
principal solar semidurnal	12.00	0.5000	2.000000	1.97
elliptical lunar semidurnal	12.66	0.5275	1.895735	1.90
declinational luni-solar				
semidiurnal	11.97	0.49875	2.005013	2.00
declinational luni-solar				
diurnal	23.93	0.997083	1.002925	1.00
principal lunar diurnal	25.82	1.075833	0.929512	0.93

Table 3:	Components	of the	C/k	spectrum	of Figure	7	compared	to	the
	harmonic con	nponent	s of	the tidal sp	pectrum.				



Figure 7: The ratio of the pollution concentration to the pollution loading rate in Great Salt Pond.

6 Conclusions

The MSB model has been used to estimate the flushing of pollution in a wellmixed tidal basin that is subjected to recreational boating activities. Key pollutants associated with recreational boating have been ascertained from studies reported in the literature. A sample analysis has been carried out for a



particular pollutant, ethylbenzene, resulting from recreational boating activities in Great Salt Pond (Block Island) for the 2004 boating season. The model is flexible enough to allow the analysis of a wide range of aqueous pollutants.

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